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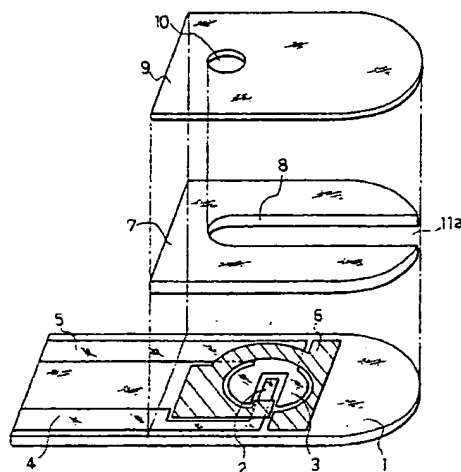
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(54) **Biosensor with C-shaped counter electrode**

(57) The biosensor has a reaction layer that contains at least an oxidoreductase and an electron acceptor and is formed on an electrode system including a working electrode and a counter electrode on a base plate. The working electrode, the counter electrode, and lead conductors connecting with these electrodes are made of carbon. The counter electrode is formed in a substantially C shape, and the working electrode is arranged between the arms of the substantially C-shaped counter electrode. An insulating layer surrounds the counter electrode and the working electrode. A cover member with a groove is combined with the base plate to define a sample supply channel that is formed therebetween and runs toward the electrode system. The groove extends from one end of the base plate and passes over the electrode system, and the insulating layer extends to an air hole formed at an end of the groove of the cover member. This arrangement prevents exposure of part of the lead conductor connecting with the working electrode to the sample solution and development of an error in measurement.

FIG. 2



Description

The present invention relates to a biosensor that is manufactured at low cost and can readily determine a specific compound in a sample at high speed and with high accuracy.

Proposed methods of quantitative analysis for determining sugars, such as sucrose and glucose, utilize a technique like polarimetry, colorimetry, reductometry, or chromatography. These methods, however, have relatively low specificity to the sugars and thereby poor accuracy. For example, the polarimetry is simple in operation but significantly affected by the peripheral temperature. Namely the polarimetry is not suitable for domestic use, in which generally non-skilled people determine sugars.

Various types of biosensors recently developed utilize the specific catalytic activities of enzymes.

The following describes determination of glucose as one example of quantitative analysis of a substrate in a sample solution. A known technique of electrochemical determination of glucose uses glucose oxidase (EC1.1.3.4; hereinafter referred to as GOD) and either an oxygen electrode or a hydrogen peroxide electrode (see, for example, 'Biosensor' ed. by Shuichi SUZUKI, Kodan-sha).

GOD uses oxygen as an electron acceptor and selectively oxidizes the substrate or β -glucose to D-glucono- δ -lactone. In the presence of oxygen, the oxidation reaction by GOD reduces oxygen to hydrogen peroxide. The decrease in amount of oxygen may be measured by the oxygen electrode, or otherwise, the increase in amount of hydrogen peroxide may be measured by the hydrogen peroxide electrode. Both the decrease in amount of oxygen and the increase in amount of hydrogen peroxide are proportional to the content of glucose in the sample solution, so that measurement of the decrease in oxygen or the increase in hydrogen peroxide determines glucose.

As presumable from its reaction process, however, this known technique has some drawbacks: the results of measurement are significantly affected by the concentration of oxygen included in the sample solution; and the absence of oxygen in the sample solution makes the measurement itself impossible.

A novel type of glucose sensor developed to remove such drawbacks uses potassium hexacyanoferrate(III), one of organic compounds such as ferrocene derivatives and quinone derivatives, or a metal complex as the electron acceptor, instead of oxygen. This novel type of sensor oxidizes the reductant of the electron acceptor obtained as a result of the enzyme reaction on the electrode and determines the concentration of glucose included in the sample solution based on the observed oxidation current. Application of the organic compound or metal complex, instead of oxygen, as the electron acceptor enables a known quantity of GOD and the electron acceptor to be accurately carried on the

electrode in a stable state to form a reaction layer. The reaction layer that is substantially in a dry state may be integrated with the electrode system. Disposal glucose sensors based on this technique have drawn much attention recently.

This disposal glucose sensor enables the user to readily determine glucose simply by introducing a sample solution into the sensor detachably connected to a measurement device. This technique is applicable to not only determination of glucose but determination of another substrate included in the sample solution.

The technique of utilizing such an electron acceptor and integrating the electrode system with the reaction layer enables simple electrochemical qualitative evaluation of the substrate. Lead conductors composed of a metal, such as palladium or silver, undesirably increase the manufacturing cost. Carbon lead conductors, on the other hand, require a relatively large width to depress an increase in electrical resistance. The large width of lead conductors causes part of a lead conductor led from a working electrode to be exposed to a sample solution, which may result in a positive error in measurement.

The present invention accordingly provides a biosensor comprising:

- a base plate with a pair of carbon lead conductors formed thereon, the carbon lead conductors having one end formed as an electrode system and the other end as an electrical connection to a measurement device;
- a cover member with a groove arranged on the base plate to define a sample supply channel that is formed therebetween and runs from one end of the base plate to the electrode system;
- an insulating layer for surrounding the electrode system on the base plate; and
- a reaction layer containing at least an oxidoreductase and an electron acceptor and being formed on the electrode system surrounded by the insulating layer, wherein the electrode system includes a substantially C-shaped counter electrode and a working electrode located in a recess of the substantially C-shaped counter electrode, the groove extending from the end of the base plate and passing over the electrode system, and the insulating layer extending to an air hole formed in a terminal of the groove of the cover member.

It is preferable that the electrical resistance between the electrode system and the electrical connection is not greater than 10 k Ω .

It is also preferable that a lecithin layer is formed in the groove of the cover member or more specifically over the whole length of the groove.

It is further preferable that the reaction layer includes a hydrophilic polymer.

Non-limiting embodiments of the present invention will now be described with reference to the accompanying drawings, in which:-

Fig. 1 is a plan view illustrating a base plate with an electrode system applied for a glucose sensor in accordance with one embodiment of the present invention; and

Fig. 2 is an exploded perspective view illustrating the glucose sensor of Fig. 1 except for a reaction layer thereof.

A working electrode 2, a counter electrode 3, and lead conductors 4 and 5 connecting with the respective electrodes are formed on an electrically insulating base plate 1. The base plate 1 is composed of polyethylene terephthalate, while the other elements 2, 3, 4, and 5 are all composed of carbon. These electrodes and lead conductors 2, 3, 4, and 5 are simultaneously formed by one-time screen printing of a binder-containing carbon paste. The counter electrode 3 is formed in a substantially C shape, and the working electrode 2 is arranged in the recess of the substantially C-shaped counter electrode 3. The lead conductors 4 and 5 connecting with these electrodes 2 and 3 extend to one end of the base plate 1, which functions as an electrical connection to a measurement device.

An electrically insulating layer 6 that is formed by printing an electrically insulating paste is further arranged on the base plate 1 with the working electrode 2, the counter electrode 3, and the lead conductors 4 and 5 formed thereon. The electrically insulating layer 6 separates the working electrode 2 and the counter electrode 3 from the lead conductors 4 and 5 and defines the exposed areas of the working electrode 2 and the counter electrode 3. It is preferable that the inner side of the electrically insulating layer 6 is formed in a substantially circular shape except a part corresponding to the working electrode 2.

A reaction layer is subsequently formed on the base plate 1 with the electrode system. The reaction layer may be readily prepared by adding solutions of required reagents dropwise onto the electrode system and drying them as discussed later. Since the carbon electrodes 2 and 3 are surrounded by the electrically insulating layer 6, the reaction layer can advantageously be formed in a restricted manner only on a specified area. In other words, the electrically insulating layer 6 prevents the solutions for forming the reaction layer from being spread to the lead conductors 4 and 5. This structure enables a homogeneous reaction layer to be prepared with high reproducibility.

A cover member is combined with the base plate 1 to define a sample supply channel formed therebetween. The cover member includes a spacer 7 with a slit 8 open to one end and a cover 9 having an air hole 10 arranged at a position corresponding to a terminal of the slit 8. The spacer 7 and the cover 9 are composed

of the same insulating material as that of the base plate 1. A biosensor is completed by bonding the base plate 1, the spacer 7, and the cover 9 to one another in such a manner that the respective portions shown by the one-dot chain lines in Fig. 2 are matched.

In this biosensor, the sample supply channel is formed in a portion 11 surrounded by the broken line in Fig. 1 on the base plate 1. The sample supply channel 11 corresponds to the slit 8 of the spacer 7 and extends over the electrode system. When an opening 11a of the sample supply channel 11 is exposed to a sample solution, the sample solution sucked by the capillary action runs through the sample supply channel 11 toward the air hole 10 and reaches the electrode system to react with the reagents of the reaction layer thereon.

As clearly shown in Fig. 1, the restricted working electrode 2 and counter electrode 3 constituting the electrode system and the electrically insulating layer 6 surrounding the electrode system are exposed on the base plate 1 facing the sample supply channel 11. The lead conductor 4 separated from the working electrode 2 by the electrically insulating layer 6 is made apart from the sample supply channel 11 by the electrically insulating layer 6. This structure effectively prevents a measurement error due to exposure of the lead conductor 4 of the working electrode 2 to the sample solution. Although part of the lead conductor 5 of the counter electrode 3 is exposed to the sample supply channel 11, the exposure of the part to the sample solution does not affect the measurement result.

Application of a paste on the working electrode, the counter electrode, and the corresponding lead conductors, which are all made of carbon, to form an electrically insulating layer often causes an increase in electrical resistance. This may be ascribed to penetration of the paste into the carbon layer. It is accordingly preferable that the electrically insulating layer for separating the working electrode and the counter electrode from their lead conductors is formed in a restricted area on the carbon printed layer as shown in Fig. 1.

In the examples discussed below, carboxymethylcellulose is used as the hydrophilic polymer. Other available hydrophilic polymers to form a hydrophilic polymer layer include hydroxyethylcellulose, hydroxypropylcellulose, methylcellulose, ethylcellulose, ethylhydroxyethylcellulose, carboxymethylethylcellulose; poly(vinyl pyrrolidone), poly(vinyl alcohol), polyamino acids such as polylysine, poly(styrene sulfonate), gelatin and its derivatives, acrylic acid and its derivatives, methacrylic acid and its derivatives, starch and its derivatives, and maleic anhydride and its derivatives. Especially preferable are carboxymethylcellulose, including hydroxyethylcellulose, hydroxypropylcellulose, methylcellulose, ethylcellulose, ethylhydroxyethylcellulose, and carboxymethylethylcellulose. Polyamino acids such as polylysine, poly(vinyl alcohol), and poly(styrene sulfonate) are also usable.

The oxidoreductase included in the reaction layer

should be varied according to the substrate to be measured. Available oxidoreductase include fructose dehydrogenase, glucose oxidase, alcohol oxidase, lactate oxidase, cholesterol oxidase, xanthine oxidase, and amino acid oxidase.

Available examples of the electron acceptor include potassium hexacyanoferrate(III), p-benzoquinone, phenazine methosulfate, methylene blue, and ferrocene derivatives. Oxygen used as the electron acceptor also ensures the sensor response. One or a plurality of these alternatives may be used for the electron acceptor.

The enzyme and the electron acceptor may be dissolved in the sample solution or may not be dissolved in the sample solution when the reaction layer is fixed to the base plate. In case that the enzyme and the electron acceptor are fixed, it is preferable that the reaction layer contains the hydrophilic polymer.

The reaction layer may further contain a pH buffer. Available pH buffers include potassium dihydrogenphosphate-dipotassium phosphate, potassium dihydrogenphosphate-disodium phosphate, sodium dihydrogenphosphate-dipotassium phosphate, sodium dihydrogenphosphate-disodium phosphate, citric acid-disodium phosphate, citric acid-dipotassium phosphate, citric acid-trisodium citrate, citric acid-tripotassium citrate, potassium dihydrogencitrate-sodium hydroxide, sodium dihydrogencitrate-sodium hydroxide, sodium hydrogenmaleate-sodium hydroxide, potassium hydrogenphthalate-sodium hydroxide, succinic acid-sodium tetraborate, maleic acid-tris(hydroxymethyl)aminomethane, tris(hydroxymethyl)aminomethane-tris(hydroxymethyl)aminomethane hydrochloride, [N-(2-hydroxyethyl)piperazine-N'-2-ethanesulfonic acid]-sodium hydroxide, [N-tris(hydroxymethyl)methyl-2-aminoethanesulfonic acid]-sodium hydroxide, and [piperazine-N,N'-bis(2-ethanesulfonic acid)]-sodium hydroxide.

Although the following examples illustrate specific printing patterns of carbon paste and an electrically insulating paste, the patterns are not restricted to these examples.

Example 1

A glucose sensor is described below as a typical example of biosensors.

The glucose sensor was manufactured in the following manner. As shown in Fig. 1, the working electrode 2, the counter electrode 3, the lead conductors 4 and 5 respectively connecting with the electrodes 2 and 3, and the electrically insulating layer 6 were formed on the base plate 1.

An aqueous solution containing GOD as the enzyme and potassium hexacyanoferrate(III) as the electron acceptor was added dropwise onto the electrode system consisting of the working electrode 2 and the counter electrode 3 and dried to form a reaction layer. Arrangement of the electrically insulating layer 6 surrounding the electrode system as shown in Fig. 1 effec-

tively prevents the solution for forming the reaction layer from being spread to the lead conductors 4 and 5.

In order to ensure smooth supply of the sample solution to the reaction layer, lecithin dissolved in an organic solvent, for example, toluene, was spread over the reaction layer and dried to form a lecithin layer. A glucose sensor was then completed by bonding the cover 9 and the spacer 7 to the base plate 1.

An aqueous glucose solution (3 μ l) as the sample solution was supplied through an opening 11a of the sample supply channel 11 of this sensor.

Simultaneously with supply of the sample solution, the reaction layer on the electrode system was dissolved in the sample solution. After 55 seconds elapsed, a predetermined potential was applied to the working electrode 2 with respect to the reference counter electrode 3. The electric current was measured after 5 seconds. The reaction of glucose with hexacyanoferrate(III) ions and GOD oxidizes glucose to gluconolactone while reducing hexacyanoferrate(III) ions to hexacyanoferrate(II) ions. The electric current for oxidizing the hexacyanoferrate(II) ion is obtained as a response. The observed electric current depended upon the concentration of glucose included in the sample solution.

Example 2

An aqueous solution of sodium carboxymethylcellulose (hereinafter referred to as CMC) was added dropwise onto the electrode system of the base plate prepared in the same manner as Example 1 and dried to form a CMC layer. An aqueous solution containing GOD as the enzyme and potassium hexacyanoferrate(III) as the electron acceptor was subsequently added dropwise onto the CMC layer and dried to form a reaction layer.

The spacer 7 and the cover 9 were bonded to each other. Lecithin dissolved in an organic solvent, for example, toluene, was added dropwise into an area of the groove in the cover member defined by the slit 8 of the spacer 7 to face the electrode system and dried to form a lecithin layer. The lecithin layer formed in the cover member ensures smooth supply of the sample solution to the reaction layer. Direct addition of the lecithin solution of organic solvent onto the reaction layer causes the solution to spread over the carbon lead conductor and may increase the electrical resistance between the electrode system and the electrical connection. Formation of the lecithin layer in the cover member, on the other hand, solves this problem.

A glucose sensor was completed by bonding the integral cover member consisting of the spacer 7 and the cover 9 with the lecithin layer to the base plate 1.

An aqueous glucose solution (3 μ l) as the sample solution was supplied through the opening of the sample supply channel 11 of this sensor. Simultaneously with supply of the sample solution, the reaction layer on the electrode system was dissolved in the sample solution.

After 55 seconds elapsed, a predetermined potential was applied to the working electrode 2 with respect to the reference counter electrode 3. The electric current was measured after 5 seconds. The observed electric current depended upon the concentration of glucose included in the sample solution.

In this example, the reaction layer contained CMC, which interfered with adsorption of the enzyme to the surface of the electrodes. This led to the better response.

Example 3

A glucose sensor was manufactured in the same manner as Example 2, except a variation in thickness of the carbon layer. A plurality of electrodes having the electrical resistances between the working electrode and the electrical connection and between the counter electrode and the electrical connection in a range of 5 to 15 k Ω were prepared by varying a thickness of the carbon layer.

The sensor response was evaluated in the same manner as Example 2. The electrodes having the resistance of not greater than 10 k Ω gave the favorable sensor response.

As discussed above, the present invention provides a biosensor that is manufactured at low cost and can readily determine a specific compound in a sample at high speed and with high accuracy.

Although the present invention has been described in terms of the presently preferred embodiments, it is to be understood that such disclosure is not to be interpreted as limiting. Various alterations and modifications will no doubt become apparent to those skilled in the art to which the present invention pertains, after having read the above disclosure. Accordingly, it is intended that the appended claims be interpreted as covering all alterations and modifications as fall within the true scope of the invention.

Claims

1. A biosensor comprising:

a base plate with a pair of carbon lead conductors formed thereon, said carbon lead conductors having first ends formed as an electrode system and second ends formed as an electrical connection for connection to a measurement device;

a cover member with a groove arranged on said base plate to define a sample supply channel that is formed therebetween and runs from one end of said base plate to said electrode system; an insulating layer for surrounding said electrode system on said base plate; and a reaction layer containing at least an oxidore-

ductase and an electron acceptor and being formed on said electrode system surrounded by said insulating layer;

wherein said electrode system comprises a substantially C-shaped counter electrode and a working electrode located in the recess between the arms of said substantially C-shaped counter electrode, said groove extending from said one end of said base plate and passing over said electrode system, and said insulating layer extending to an air hole formed at an end of said groove of said cover member.

2. The biosensor in accordance with claim 1, wherein electrical resistance between said electrode system and said electrical connection is not greater than 10 k Ω .
3. The biosensor in accordance with either one of claims 1 and 2, wherein a lecithin layer is formed in said groove of said cover member.
4. The biosensor in accordance with any one of claims 1 through 3, wherein said reaction layer comprises a hydrophilic polymer.

FIG. 1

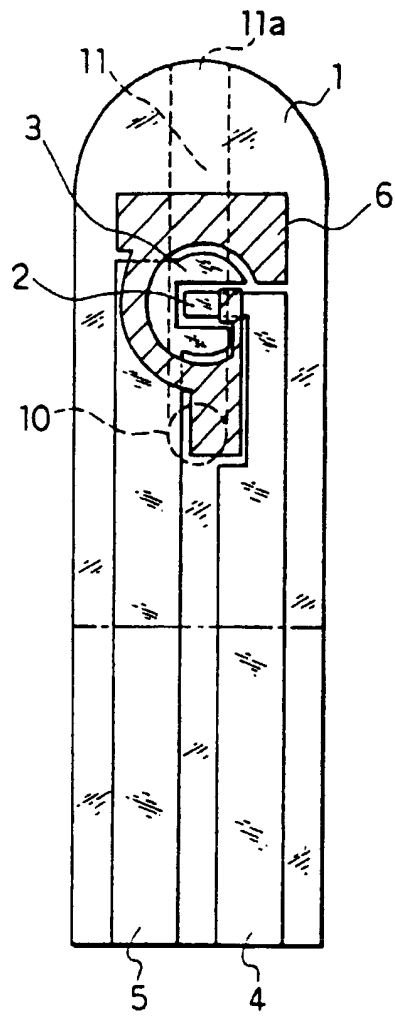
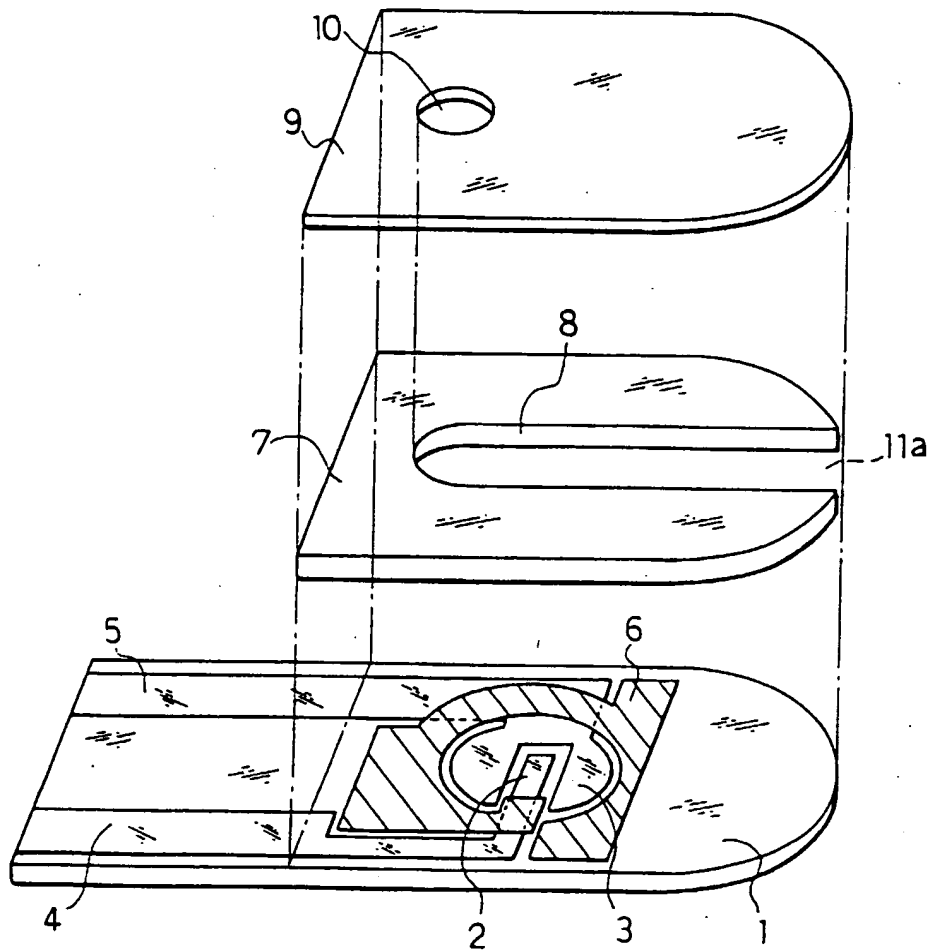


FIG. 2





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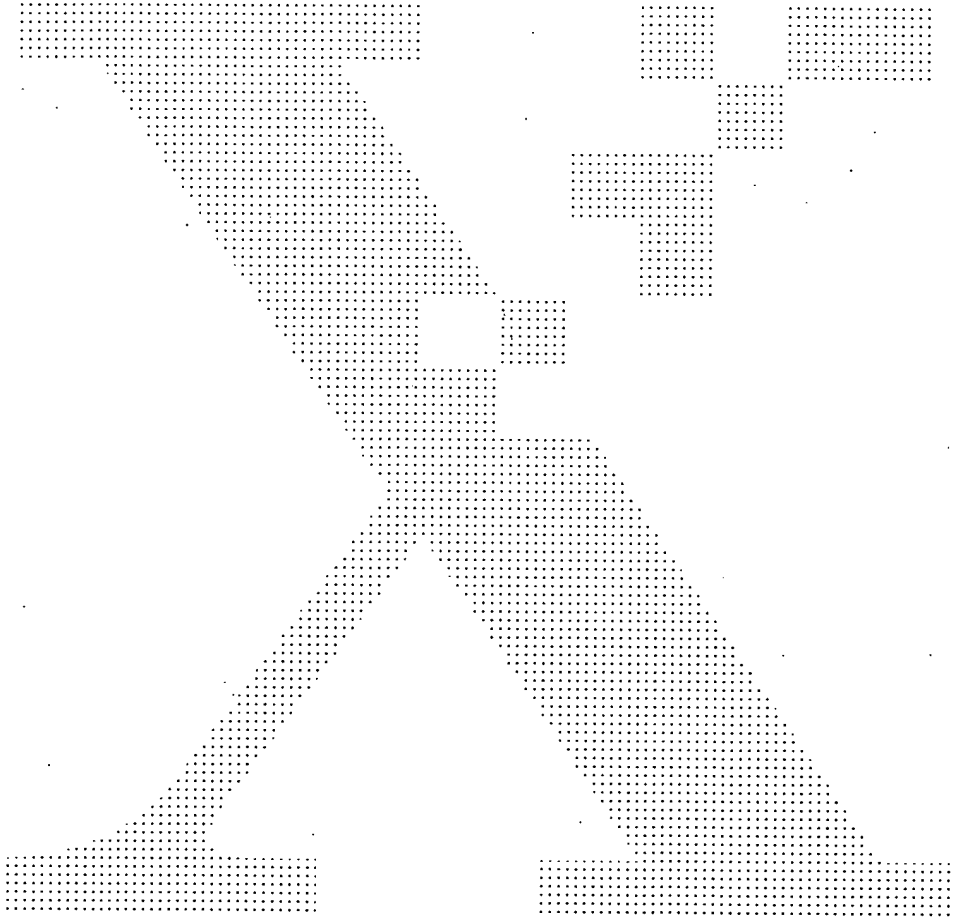
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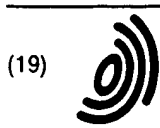
DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
X	EP 0 732 406 A (MATSUSHITA ELECTRIC IND CO LTD) * the whole document *	1	G01N27/327 C12Q1/00
A	EP 0 735 363 A (MATSUSHITA ELECTRIC IND CO LTD) * the whole document *	1	
A	EP 0 537 761 A (MATSUSHITA ELECTRIC IND CO LTD) * the whole document *	1	
			TECHNICAL FIELDS SEARCHED (Int.Cl.6)
			C12Q G01N
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 26 March 1998	Examiner Moreno, C
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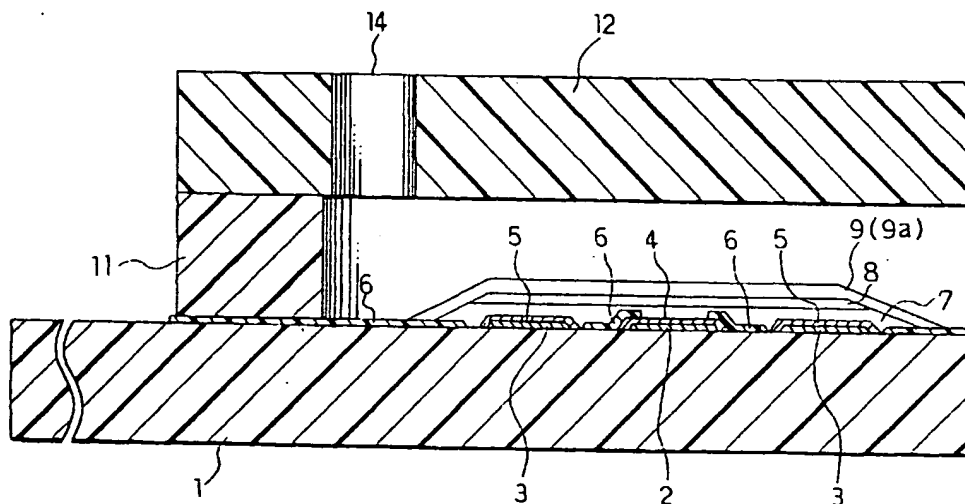
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(54) Biosensor and method of manufacturing the same

(57) Disclosed is a biosensor facilitating high accuracy quantification of a specific component in a sample solution with no adverse influence of solid substances. The biosensor comprises an electrically insulating base plate, an electrode system comprising a working elec-

trode and a counter electrode formed on the base plate, a reaction layer containing at least one enzyme disposed on the electrode system, and an anionic filter formed on the reaction layer for inhibiting permeation of solid components.

FIG. 2



EP 0 856 586 A1

Description

The present invention relates to a biosensor for rapid and high accuracy quantification of a specific component contained in a sample and a method of manufacturing the same.

Conventionally, there is a disclosure of a biosensor as mentioned below as the system for facilitating simplified quantification of a specific component contained in a sample without necessitating dilution or agitation of the sample solution (Japanese Laid-Open Patent Publication Hei 3-202764).

More specifically, the biosensor is manufactured by forming an electrode system comprising a working electrode and a counter electrode on an electrically insulating base plate by screen printing and the like, and subsequently forming thereon an enzyme reaction layer comprising a hydrophilic polymer, an oxidoreductase, and an electron acceptor.

If a sample solution containing a substrate is dropped on the enzyme reaction layer of the biosensor thus produced, the enzyme reaction layer is dissolved, causing reaction between the substrate and the enzyme. As a result, the substrate is oxidized and, at the same time, the electron acceptor is reduced. Upon completion of the substrate-enzyme reaction, the reduced electron acceptor is electrochemically oxidized. The concentration of the substrate in the sample solution is then determined from the current value across the electrodes during this oxidation reaction.

The biosensor having the above-mentioned structure, however, has a drawback that even if the concentration of the substrate in the sample solution is equal, there arises a difference in the measured oxidation current value depending on other components contained in the sample solution.

One possible cause is interaction between solid substances exceeding 1 μm in size, such as hemocyte contained in the sample solution, and the electron acceptor reduced upon enzyme-substrate reaction. Close contact of the solid substances with the reduced electron acceptor will cause oxidation of the electron acceptor by the interaction therebetween, which leads to inaccurate measurement of the oxidation current value.

One effective measure for correcting this issue is to dilute the sample solution with a certain dilute solution in order to minimize the difference in the nature of the components contained in the sample solution. This method, however, is not necessarily advisable from the aspect of operability or controllability.

The object of the present invention is to provide a biosensor which can reduce or overcome the above-mentioned problems.

The present invention provides a biosensor comprising an electrically insulating base plate, an electrode system having a working electrode and a counter electrode formed on the base plate, a reaction layer containing at least an enzyme disposed on the electrode sys-

tem, and an anionic filter formed over the reaction layer for the purpose of inhibiting permeation of solid components.

In a preferred mode of the present invention, the anionic filter is composed of a porous film made of a film-forming polymer or a fiber sheet made by a paper machine, and an anionic polymer supported on the porous film or fiber sheet.

In another preferred mode of the present invention, the anionic filter is a porous film made of a mixture of a film-forming polymer and an anionic polymer.

According to the present invention, it is possible to provide a biosensor which facilitates high accuracy quantification of a substrate in a sample solution with no adverse effects of solid components coexisting with the substrate.

Non-limiting embodiments of the present invention will now be described with reference to the accompanying drawings, in which:-

FIG. 1 shows an exploded perspective view of a biosensor in one example of the present invention, with omission of a reaction layer; and

FIG. 2 shows a longitudinal cross-sectional view illustrating the parts of the biosensor.

The anionic filter in accordance with the present invention may be composed of a combination of a filter for restricting movements of solid components in a sample solution and an anionic polymer for inhibiting dispersion of the electron acceptor contained in the reaction layer into the sample solution.

As the movement restricting filter, a porous film formed from a film-forming polymer or a glass fiber sheet made by a paper machine, a cellulose fiber or a resin fiber is preferable.

The preferable method for imparting an anionic property to the filter is to support an anionic polymer on the porous film or fiber sheet. It is also preferred to form the porous film from a mixture of a film-forming polymer and an anionic polymer.

As the measure for imparting the filter with the anionic property to obtain an anionic filter, it is preferable to contain the anionic polymer by not less than 5 wt% of the filter.

If the polymer used has the anionic as well as film-forming properties at the same time, then an anionic filter can be formed by using only this polymer.

The anionic filter in accordance with the present invention has two different functions as follows.

First, the smaller pore size of the anionic filter than the solid components in the sample solution prevents infiltration of solid components into the reaction layer.

Second, electrostatic repulsion of the anionic polymer contained in the anionic filter for the electron acceptor (which is an anionic compound) contained in the reaction layer inhibits dispersion of the electron acceptor in the sample solution beyond the filter.

The anionic filter separates the electron acceptor in the reaction layer from the solid components in the sample solution by the above-noted two functions. As a result, oxidation of the electron acceptor which has been reduced upon enzyme-substrate reaction by the solid components in the sample solution can be prevented, and the adverse effect of the solid components on the sensor response can be minimized.

In order to express the first function, the anionic filter preferably has a pore size of not more than 1 μm to avoid permeation of solid components, such as hemocyte, for example, which are contained in the sample solution and will cause adverse effects on the sensor response.

As the film-forming polymer for constituting the anionic filter, at least one selected from the group consisting of ethyl cellulose, methyl cellulose, hydroxypropyl cellulose, cellulose acetate, nitrocellulose, polyvinyl pyrrolidone, polysulfon, polyvinylidene fluoride, polyamide and polyimide is preferably used.

As the anionic polymer which is another constituent for the anionic filter, at least one selected from the group consisting of polymers having at the side chain thereof a sulfonyl group, a sulfonic acid group or a carboxyl group is preferably used. The polymers may be exemplified as perfluorosulfonate ionomer, perfluorocarboxylate ionomer, polyacrylic acid, polymethacrylic acid, polyvinyl sulfate, polystyrene sulfonate, polyglutamic acid, polyaspartic acid, and carboxymethylcellulose.

The method of manufacturing a biosensor in accordance with the present invention comprises the steps dropping a solution containing a hydrophilic polymer over an electrode system disposed on an electrically insulating base plate and drying the solution to form a hydrophilic polymer layer on the electrode system, dropping a solution containing at least one enzyme on the hydrophilic polymer layer and drying the solution to form a reaction layer on the hydrophilic polymer layer, and forming an anionic filter for covering the reaction layer.

If the solution containing the enzyme is not agitated after dropping it on the hydrophilic polymer layer in the step of forming the reaction layer, the hydrophilic polymer layer would not be mixed with the enzyme layer, so that the surface of the electrode system can be covered with only the hydrophilic polymer layer. This prevents easy development of adverse changes in the performance of the electrode system due to adsorption of proteins onto the surface of the electrode system or chemical reaction caused by an oxidizing substance, such as electron acceptor which is sometimes contained in the reaction layer. Furthermore, since this structure increases dissolution of the reaction layer, a sensor response with high accuracy can be obtained.

The aforementioned anionic filter is formed by the four methods as exemplified below.

1. To form the anionic filter by the steps of disposing a medium dissolved or dispersed therein with a film-forming polymer on the reaction layer and drying the

solution to form a filter, impregnating the filter formed from the film-forming polymer with a medium dissolved or dispersed therein with an anionic polymer to allow sufficient infiltration of the medium into the filter, and then drying the filter to obtain an anionic filter imparted with the anionic property.

At that time, it is preferable to select a medium which would not dissolve the filter formed from the film-forming polymer as the medium used for dissolving or dispersing the anionic polymer.

2. To form the anionic filter by the step of disposing a medium dissolved or dispersed therein with a film-forming polymer and an anionic polymer on the reaction layer and drying the medium.

3. To form the anionic filter by the steps of cutting a fiber sheet to a size which is large enough to cover the entire surface of the reaction layer and adhering it with pressure onto the reaction layer, impregnating the filter with a medium dissolved or dispersed therein with an anionic polymer to allow sufficient infiltration of the medium into the filter, and then drying the filter to obtain an anionic filter imparted with the anionic property.

4. To form the anionic filter by the steps of forming an anionic filter previously, then cutting the anionic filter to a size which is large enough to cover the entire surface of the reaction layer, and adhering it with pressure onto the reaction layer. As the anionic filter used here, one formed in advance on a base or the like different from the electrically insulating base plate by either method from 1 to 3 may be used. This method is useful if the medium in which at least one of the film-forming polymer and the anionic polymer is dissolved or dispersed is such a medium that could dissolve the reaction layer.

The step of disposing various mediums on the reaction layer, or impregnating the filter with those mediums is preferably performed by dropping, or immersion.

As the solvent for dissolving the anionic polymer, one selected from the group consisting of water, methanol, ethanol, propanol, butanol, acetone, toluene, xylene and ethyl ether, or a mixture of two or more of them is used preferably. The preferable choice is a solvent which would not dissolve the filter or the reaction layer formed.

As the enzyme contained in the reaction layer, either of glucose oxidase, glucose dehydrogenase, lactate oxidase, lactate dehydrogenase, fructose dehydrogenase, galactose oxidase, cholesterol oxidase, cholesterol dehydrogenase, cholesterol esterase, alcohol dehydrogenase, alcohol oxidase, ascorbate oxidase, bilirubin oxidase, or the like may be selected, depending on the measuring substrate of target.

Accordingly, the biosensor in accordance with the present invention is of wide applicability as a biosensor, such as glucose sensor, alcohol sensor, sucrose sensor, cholesterol sensor, lactose sensor, fructose sensor, and

the like, which use an enzyme-associated reaction system.

As the electron acceptor, at least one selected from potassium ferricyanide, p-benzoquinone, phenazine methosulfate, indophenol and derivatives thereof, β -naphthoquinone-4-potassium sulfonate, methylene blue, and ferrocene and derivatives thereof is used.

As the hydrophilic polymer, at least one selected from carboxymethylcellulose, hydroxyethyl cellulose, hydroxypropyl cellulose, carboxyethylmethyl cellulose, polyvinyl pyrrolidone, polyvinyl alcohol, gelatin and derivatives thereof, polyacrylic acid, polyacrylates, polymethacrylic acid, polymethacrylates, starch and derivatives thereof, and polymers containing maleic anhydride or its salts is used.

As the solvent for dissolving the enzyme, the electron acceptor and the hydrophilic polymer, water or various buffer solutions including phosphate buffer solution, citrate buffer solution, acetate buffer solution, tris-hydrochloride buffer solution and the like may be used.

There are two methods for reacting the enzyme with the substrate: 1) by dissolving the reaction layer containing an enzyme in a sample solution containing a substrate to cause reaction between the enzyme and the substrate, and 2) by solidifying the reaction layer to prevent it from floating on the sample solution, thereby causing reaction between the enzyme and the substrate just upon the surface of the reaction layer.

The anionic filter in accordance with the present invention is also effective for such a biosensor that utilizes oxygen present in the sample solution as the electron acceptor due to the type of electrodes included.

The method of measurement of oxidation current includes two-electrode system comprising a measuring electrode and a counter electrode and three-electrode system further comprising a reference electrode; the latter permits more accurate measurement.

In the following, the present invention will be described more specifically by way of concrete examples. FIG. 1 is a broken oblique perspective view of a biosensor with omission of a reaction layer. A biosensor is assembled by joining an electrically insulating base plate 1 disposed with an electrode system, cover 12 provided with an air vent 14 and a spacer 11 in a positional relationship as shown by the dotted line in FIG. 1.

In the biosensor thus obtained, since a cavity for constituting a sample solution supply pathway is formed in a slit 15 of the spacer 11 between the base plate 1 and the cover 12, a sample solution can be introduced into the reaction layer readily through the sample solution supply pathway by simply contacting the sample solution with a tip 13 of the slit 15 serving as an opening. With this structure, the supply amount of the sample solution depends on the volume of the cavity formed by the cover 12 and the spacer 11, so that pre-quantification of the sample solution is unnecessary. In addition, this structure minimizes evaporation of the sample solution during measurement, facilitating high accuracy

measurement. The use of a transparent polymer material for the cover and the spacer permits easy observation of the conditions of the reaction layer and introduction of the sample solution from the outside.

FIG. 2 shows a longitudinal cross-sectional view of the biosensor in accordance with the present invention.

First, the electrically insulating base plate 1 is provided with leads 2 and 3 by screen-printing a silver paste thereon. The base plate 1 is further disposed thereon with an electrode system comprising a working electrode 4 and a counter electrode 5 each made of a conductive carbon paste containing a resin binder, and an electrically insulating layer 6 made of an electrically insulating paste. The layer 6 has two functions to hold the areas where the working electrode 4 and the counter electrode 5 are exposed constant, and to cover part of the leads. Then, a hydrophilic polymer layer 7 is formed on the electrode system. Subsequently, an enzyme layer 8 is formed on the hydrophilic polymer layer 7. The two layers thus formed are then covered with an anionic filter 9 or a filter 9a. The enzyme layer 8 further contains an electron acceptor depending on the material used for the electrode system.

Example 1

First, a 0.5 wt% aqueous solution of sodium salt of carboxymethylcellulose (hereinafter abbreviated to "CMC") was dropped over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 and dried at 50 °C for 10 minutes in a hot drier to form the hydrophilic polymer layer 7 (CMC layer). Subsequently, a mixture aqueous solution containing glucose oxidase (EC1.1.3.4; hereinafter abbreviated to "GOD") at 10 mg/ml and potassium ferricyanide at 16 mg/ml was prepared. The mixture aqueous solution thus prepared was dropped over the CMC layer 7 and dried at 50 °C for another 10 minutes in a hot drier to form the enzyme layer 8.

Then, a mixture ethanol solution A was formulated by mixing a 2 wt% ethanol solution of ethyl cellulose and a 0.5 wt% ethanol solution of hydroxypropyl cellulose. An aliquot of 5 μ l of the mixture ethanol solution A was dropped on the enzyme layer 8 and dried for 10 minutes at room temperature to form a filter comprising a film-forming polymer. Then, for imparting the filter thus formed with an anionic property, an aliquot of 5 μ l of a 1 wt% butanol solution of perfluorosulfonate ionomer was dropped on the filter and dried at 50 °C for 10 minutes. This gave the anionic filter 9.

Finally, the cover 12 and the spacer 11 were adhered to the base plate 1 in the positional relationship as shown by the dotted line in FIG. 1. In this way, a glucose sensor of this example was produced.

Separately, a blood sample solution and a glucose aqueous solution for this glucose sensor were prepared by adjusting the concentration of glucose in each solution equal. An aliquot of 3 μ l of each sample solution

was supplied from the opening 13 of the sample solution supply pathway.

After introduction through the opening 13, the sample solution reaches the air vent 14 and infiltrates the anionic filter 9. The solution which has passed through the anionic filter causes dissolution of the reaction layer. In the reaction layer, the glucose contained in the sample solution is oxidized by the glucose oxidase present in the reaction layer, which causes electron movement, and the electron moved reduces potassium ferricyanide to potassium ferrocyanide.

One minute after introduction of the sample solution, a voltage of +0.5 V on the basis of the voltage of the counter electrode 5 was applied to the working electrode 4 and the anodic current value was measured after 5 seconds. The measurement results showed that the current value in response to the blood sample solution was about 98% of that in response to the glucose aqueous solution.

Example 2

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, an aliquot of 5 μ l of the mixture ethanol solution A, which was prepared in Example 1, was dropped on the enzyme layer 8 and dried for 10 minutes at room temperature to form a filter comprising a film-forming polymer. Subsequently, for imparting the anionic property to this filter, an aliquot of 5 μ l of a 1 wt% aqueous solution of polyacrylic acid was dropped on the filter and dried at 50 °C for 10 minutes. This gave the anionic filter 9.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 95% of that in response to the glucose aqueous solution.

Example 3

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, a mixture ethanol solution B was formulated by mixing a 2 wt% ethanol solution of ethyl cellulose and a 0.2 wt% ethanol solution of perfluorocarboxylate ionomer. An aliquot of 5 μ l of the mixture ethanol solution B was dropped on the enzyme layer 8 and dried for 10 minutes at room temperature to form the anionic filter 9.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and

the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 97% of that in response to the glucose aqueous solution.

Example 4

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, a glass fiber sheet was cut to a size which is large enough to cover the entire surface of the reaction layer and adhered with pressure to the reaction layer to form a filter. Subsequently, an aliquot of 10 μ l of a 0.5 wt% ethanol solution of perfluorosulfonate ionomer was dropped on the filter and dried for 10 minutes at room temperature. In this way, the filter was imparted with the anionic property and the anionic filter 9 was obtained.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 98% of that in response to the glucose aqueous solution.

Example 5

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, the anionic filter 9 was formed in the same manner as in Example 4, except for the use of a cellulose fiber sheet in place of the glass fiber sheet.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 95% of that in response to the glucose aqueous solution.

Example 6

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, a filter was formed in the same manner as in Example 4 by adhering with pressure a cellulose fiber sheet to the reaction layer. Subsequently, a 1% aqueous solution of polyacrylic acid was formulated and an aliquot of 10 μ l of the solution was dropped on the filter and dried at 50 °C for 10 minutes, which gave the anionic filter 9.

Finally, a glucose sensor of this example was pro-

duced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 97% of that in response to the glucose aqueous solution.

Example 7

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, an aliquot of 5 μ l of the mixture ethanol solution B, which was prepared in Example 3, was dropped on a glass plate and dried for 10 minutes at room temperature to form the anionic filter 9 composed of a mixture of a film-forming polymer and an anionic polymer. Subsequently, the filter thus formed was peeled off from the glass plate, then cut to a size which is large enough to cover the entire surface of the enzyme layer 8, and adhered with pressure to the enzyme layer 8.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 95% of that in response to the glucose aqueous solution.

Example 8

In this example, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, a glass fiber filter was immersed in a 2% ethanol solution of perfluorosulfonate ionomer, and then dried at room temperature for 10 minutes, followed by further drying at 50 °C for another 5 minutes in a hot drier. In this way, the glass fiber filter was imparted with the anionic property and an anionic filter was obtained. Subsequently, the anionic filter thus formed was cut to a size which is large enough to cover the entire surface of the reaction layer, and adhered with pressure to the reaction layer.

Finally, a glucose sensor of this example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 95% of that in response to the glucose aqueous solution.

Comparative Example 1

For comparison, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode sys-

tem disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1, except for omission of the anionic filter 9.

Then, a glucose sensor of this comparative example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 70 to 80% of that in response to the glucose aqueous solution.

Comparative Example 2

For comparison, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, an aliquot of 5 μ l of a 2 wt% ethanol solution of ethyl cellulose was dropped on the enzyme layer 8 and dried for 10 minutes at room temperature to form the filter 9a. The filter 9a comprising a film-forming polymer was not imparted with the anionic property.

Finally, a glucose sensor of this comparative example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 83% of that in response to the glucose aqueous solution.

Comparative Example 3

For comparison, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, an aliquot of 5 μ l of a 0.1 wt% ethanol solution of perfluorosulfonate ionomer was dropped on the enzyme layer 8 and dried for 10 minutes at room temperature. In this way, an anionic polymer was adhered to the enzyme layer 8.

Finally, a glucose sensor of this comparative example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 73% of that in response to the glucose aqueous solution.

Comparative Example 4

For comparison, the hydrophilic polymer layer 7 and the enzyme layer 8 were formed over the electrode system disposed on the electrically insulating base plate 1 as shown in FIG. 2 in the same manner as in Example 1.

Then, a glass fiber sheet was adhered to the reaction layer with pressure in the same manner as in Ex-

ample 4 to form the filter 9a on the reaction layer. The filter 9a was not imparted with the anionic property.

Finally, a glucose sensor of this comparative example was produced in the same manner as in Example 1, and the sensor responses to the glucose aqueous solution and the blood sample solution were measured. The measurement results showed that the current value in response to the blood sample solution was about 80% of that in response to the glucose aqueous solution.

Although the present invention has been described in terms of the presently preferred embodiments, it is to be understood that such disclosure is not to be interpreted as limiting. Various alterations and modifications will no doubt become apparent to those skilled in the art to which the present invention pertains, after having read the above disclosure. Accordingly, it is intended that the appended claims be interpreted as covering all alterations and modifications as fall within the true scope of the invention.

Claims

1. A biosensor comprising an electrically insulating base plate, an electrode system having a working electrode and a counter electrode formed over said base plate, a reaction layer containing at least an enzyme disposed on said electrode system, and an anionic filter formed over said reaction layer for inhibiting permeation of solid components.
2. The biosensor in accordance with claim 1, wherein said anionic filter is composed of a porous film made of a film-forming polymer or a fiber sheet, and an anionic polymer supported on said porous film or fiber sheet.
3. The biosensor in accordance with claim 1, wherein said anionic filter is a porous film made of a mixture of a film-forming polymer and an anionic polymer.
4. The biosensor in accordance with claim 2 or 3, wherein said film-forming polymer is at least one selected from the group consisting of ethyl cellulose, methyl cellulose, hydroxypropyl cellulose, cellulose acetate, nitrocellulose, polyvinyl pyrrolidone, polysulfon, polyvinylidene fluoride, polyamide and polyimide, and said anionic polymer is at least one selected from the group consisting of polymers having at the side chain thereof at least one functional group selected from the group consisting of a sulfonyl group, a sulfonate group and a carboxyl group.
5. A method of manufacturing a biosensor comprising the steps of:

dropping a solution containing a hydrophilic polymer on an electrode system disposed on

an electrically insulating base plate and drying said solution to form a hydrophilic polymer layer on said electrode system, dropping a solution containing at least one enzyme on said hydrophilic polymer layer and drying the solution to form a reaction layer on said hydrophilic polymer layer, and forming an anionic filter for covering said reaction layer.

6. The method of manufacturing a biosensor in accordance with claim 5, wherein the step of forming said anionic filter comprises the steps of:

disposing a medium dissolved or dispersed therein with a film-forming polymer on said reaction layer and drying the medium to form a filter, and

impregnating said filter with a medium dissolved or dispersed therein with an anionic polymer and drying the filter to form an anionic filter imparted with an anionic property.

7. The method of manufacturing a biosensor in accordance with claim 6, wherein said medium for dissolving or dispersing said anionic polymer is one that would not dissolve said film-forming polymer.

8. The method of manufacturing a biosensor in accordance with claim 5, wherein the step of forming said anionic filter comprises the step of disposing a mixture dissolved or dispersed therein with a film-forming polymer and an anionic polymer on said reaction layer and drying the mixture to form an anionic filter.

9. The method of manufacturing a biosensor in accordance with claim 5, wherein the step of forming said anionic filter comprises the steps of:

adhering with pressure a fiber sheet onto said reaction layer to form a filter, and

impregnating said filter with a medium dissolved or dispersed therein with an anionic polymer and drying the filter to obtain an anionic filter imparted with an anionic property.

10. The method of manufacturing a biosensor in accordance with claim 5, wherein the step of forming said anionic filter comprises the step of adhering with pressure a pre-fabricated anionic filter onto said reaction layer.

FIG. 1

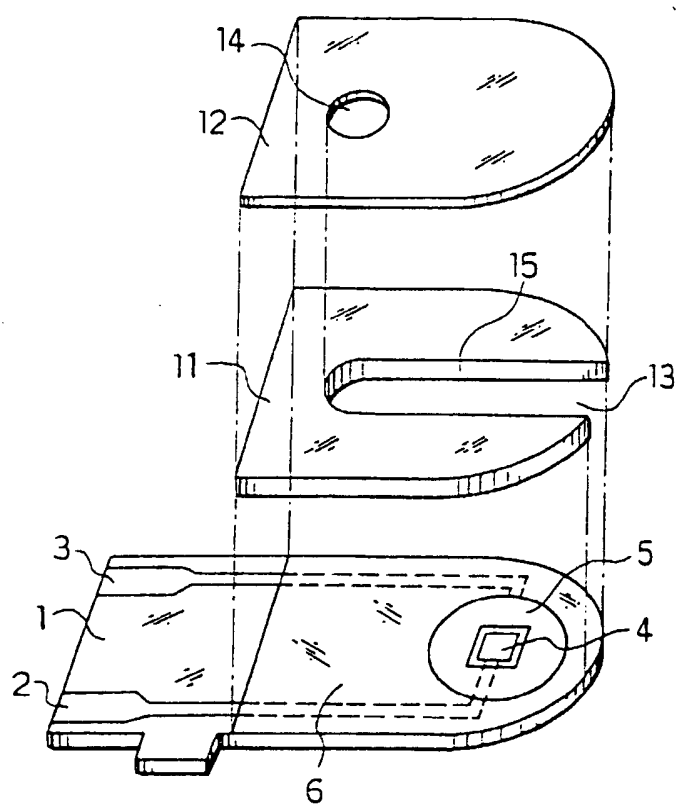
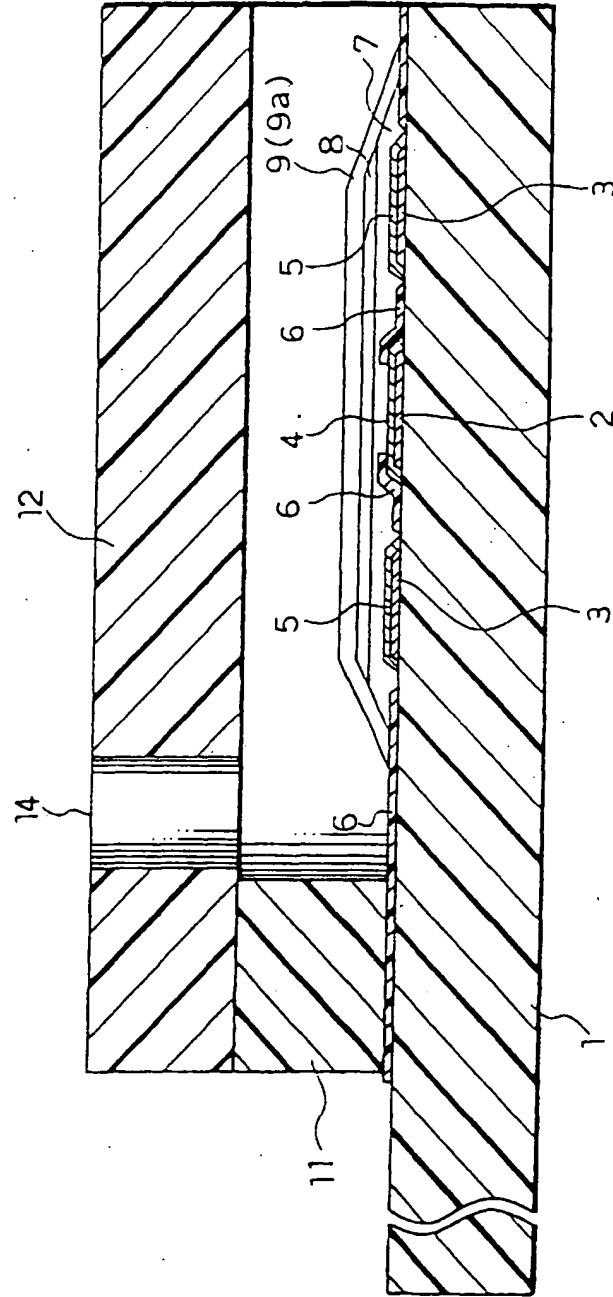


FIG. 2





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EUROPEAN SEARCH REPORT

Application Number
EP 98 30 0273

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Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
Y	US 5 512 159 A (YOSHIOKA TOSHIHIKO ET AL) 30 April 1996 * column 4, line 1-30; claim 1 *	1,5	C12Q1/00 G01N27/327
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A	EP 0 470 290 A (SIEMENS AG) 12 February 1992 * abstract *	1	
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A	EP 0 685 737 A (MATSUSHITA ELECTRIC IND CO LTD) 6 December 1995 * claims 1-17 *	1,5	TECHNICAL FIELDS SEARCHED (Int.Cl.6) C12Q G01N
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The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 15 May 1998	Examiner Brison, O
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons a : member of the same patent family, corresponding document	

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Application Number
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The present search report has been drawn up for all claims			
Place of search BERLIN		Date of completion of the search 15 May 1998	Examiner Brison, O
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